

# A 2.4 GHz FREQUENCY SELECTIVE BACKSCATTER MODULATOR FOR BLUETOOTH AND WI-FI BACKSCATTER

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## Background and Motivation

- Backscatter devices used in many Internet of Things (IoT) applications<sup>1-4</sup>
- Adoption of ultra-low power backscatter modulators (**BSMs**) has potential to dramatically reduce creation of hazardous battery waste
- Open problem:** a single BSM scatters energy from all nearby sources in the environment → leads to spectral pollution and potential for interference with other nearby communication links
- Our approach:** add in-line band-pass filter (BPF) to create a **frequency selective (FS) BSM**, which preferentially modulates signals within BPF's passband, regardless of antenna's bandwidth (BW)
- In Bluetooth (BT) or Wi-Fi context, our approach could allow backscatter within only the 2.4 GHz ISM band, or ideally within 20 MHz bandwidth of a single Wi-Fi channel

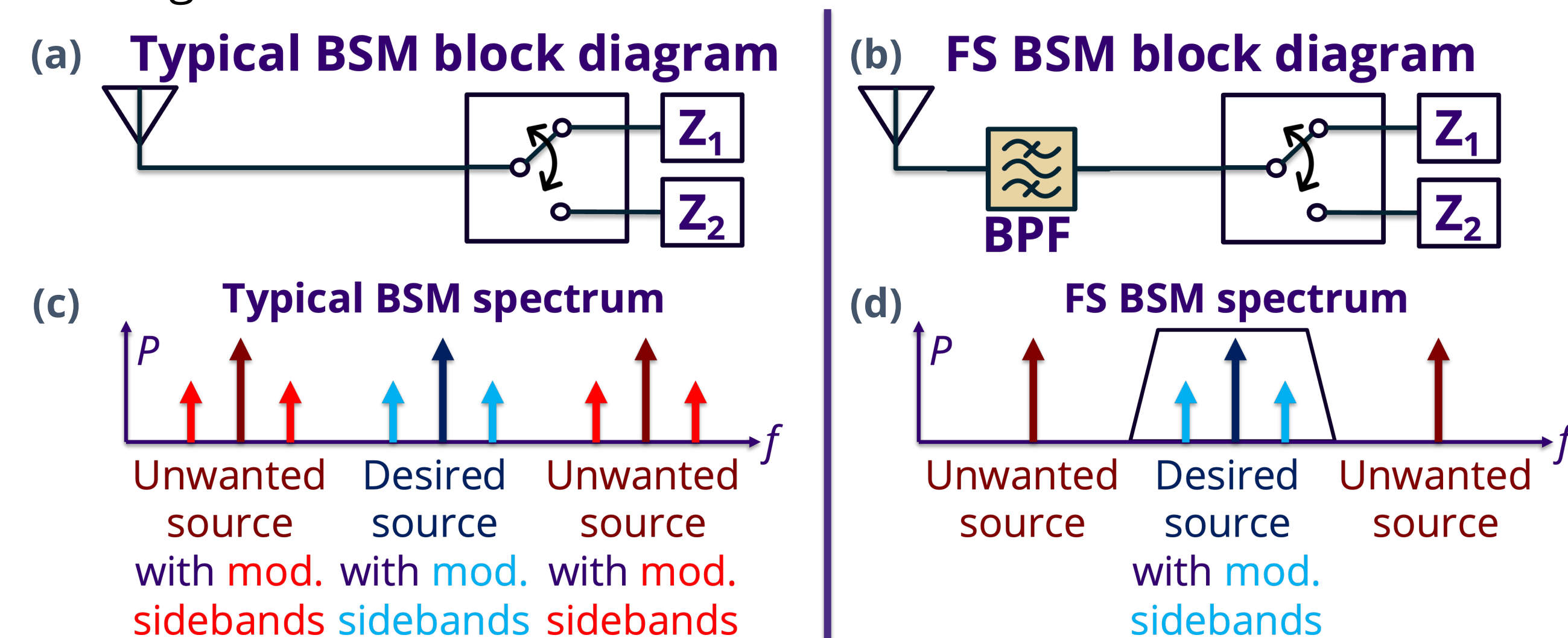
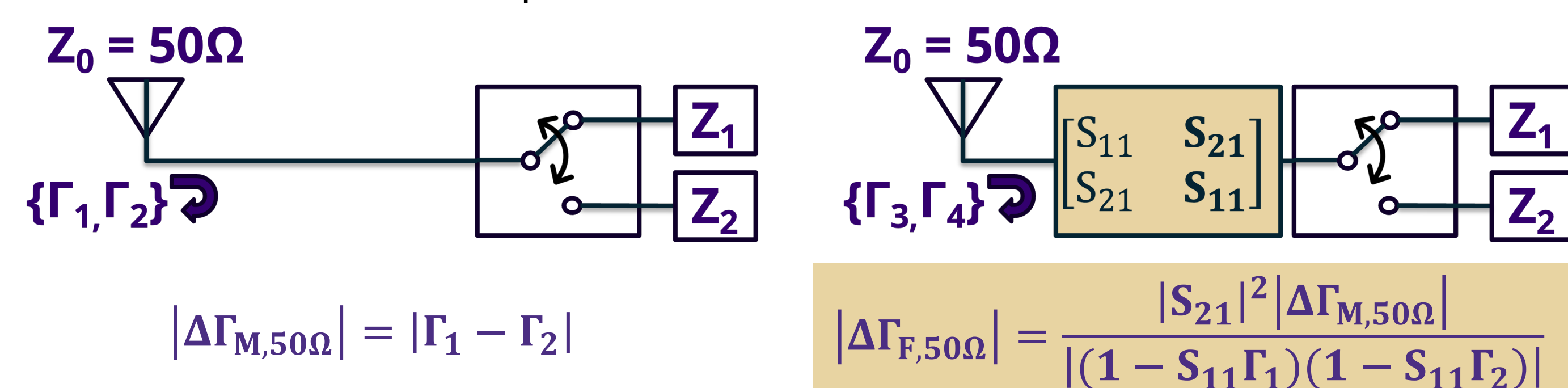


Fig. 1: Block diagram of (a) a typical BSM and (b) the proposed FS BSM. Spectrum of (c) a typical BSM, including unwanted backscatter modulation of out-of-band carriers, and (d) the proposed FS BSM. The addition of a BPF ensures scattering from carriers in the desired band.

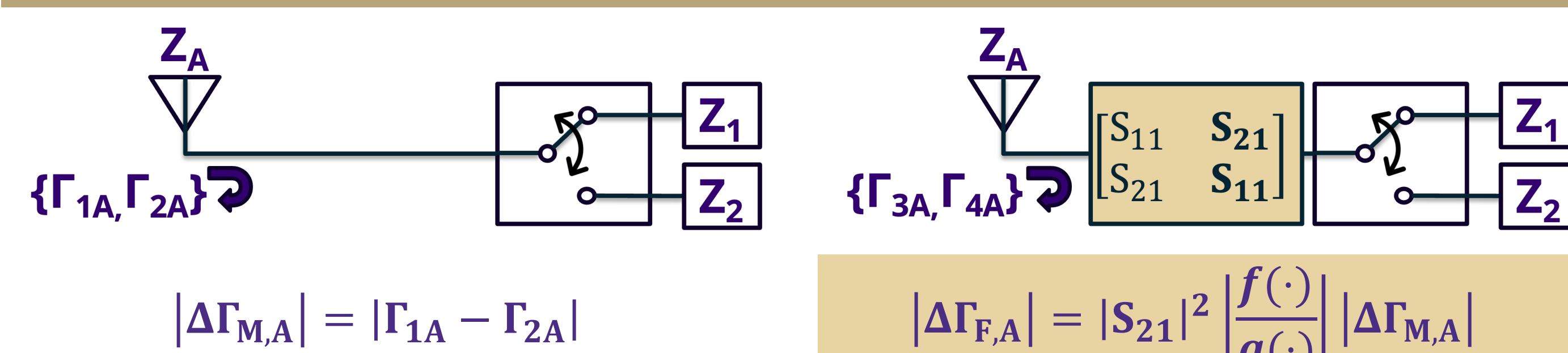
## Engineering Frequency Selectivity

The frequency-dependent **differential reflection coefficient**,  $|\Delta\Gamma|$ , is used to characterize amount of modulated backscatter.  $|\Delta\Gamma|$  ranges from 0 to 2 for minimum to maximum backscatter and is computed as the difference between complex-valued reflection coefficients.



- Adding reciprocal 2-port network yields a new, **filtered**  $|\Delta\Gamma_{50\Omega}|$ , which is a scaled version of the original
- An ideal BPF enables **frequency selective**  $|\Delta\Gamma_{F,50\Omega}|$ .
  - **Stopband:**  $|S_{11}| = 1$  and  $|S_{21}| = 0 \rightarrow |\Delta\Gamma_{F,50\Omega}| = 0$ .
  - **Passband:**  $|S_{11}| = 0$  and  $|S_{21}| = 1 \rightarrow |\Delta\Gamma_{F,50\Omega}| = |\Delta\Gamma_{M,50\Omega}|$

## Practical Considerations



- In practice, an antenna having complex impedance  $Z_A \neq 50\Omega$  is used
- After converting each  $50\Omega$ -ref'd  $\Gamma_n$  into its respective impedance parameter,  $Z_n$ , the corresponding reflection coefficient seen by the antenna is found as:  $\Gamma_{nA} = \frac{Z_n - Z_A^*}{Z_n + Z_A}$ ,  $n \in \{1, 2, 3, 4\}$

Crucially, an ideal BPF can also **enable frequency selective**  $|\Delta\Gamma_{F,A}|$

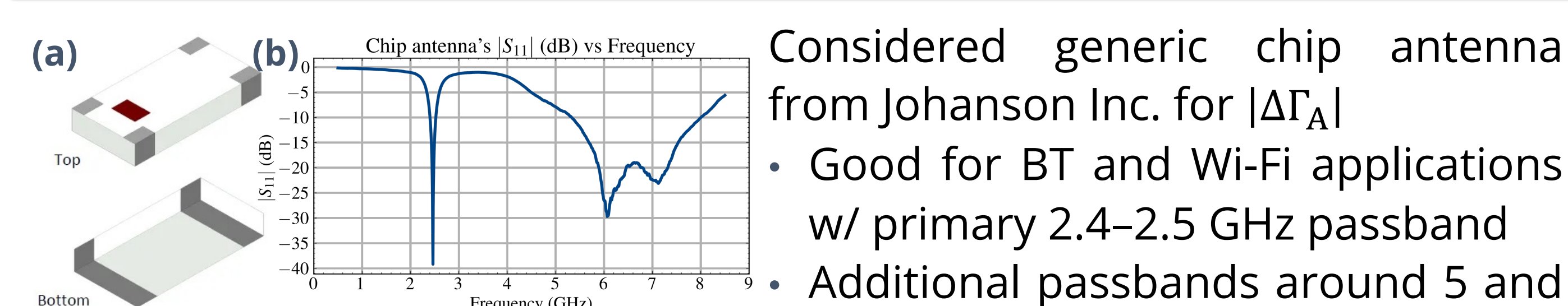


Fig. 2: (a) diagram and (b)  $|S_{11}|$  of antenna 6 GHz

## Experimental Validation

All three devices evaluated are commonly used in backscatter applications<sup>5</sup> and compatible with 0-5V logic levels of Arduino Nano microcontroller:

- Varactor:** voltage tunes Cap. from 36 pF to 2.7 pF
- PIN diode:** open- or short-circuit when rev. or fwd. biased
- pHEMT:** open- or short-circuit as gate driven low or high

Paired with two filter types:

- Off-the-shelf low-temperature co-fired ceramic (**LTCC**) BPF
- Microstrip custom filter (**CF**) = Stepped-impedance low-pass filter (LPP) + microstrip coupled line BPF (MCFIL)

Designed and fabricated FR-4 printed circuit board (PCB) for microstrip CF, and three FR-4 PCBs for the modulators.

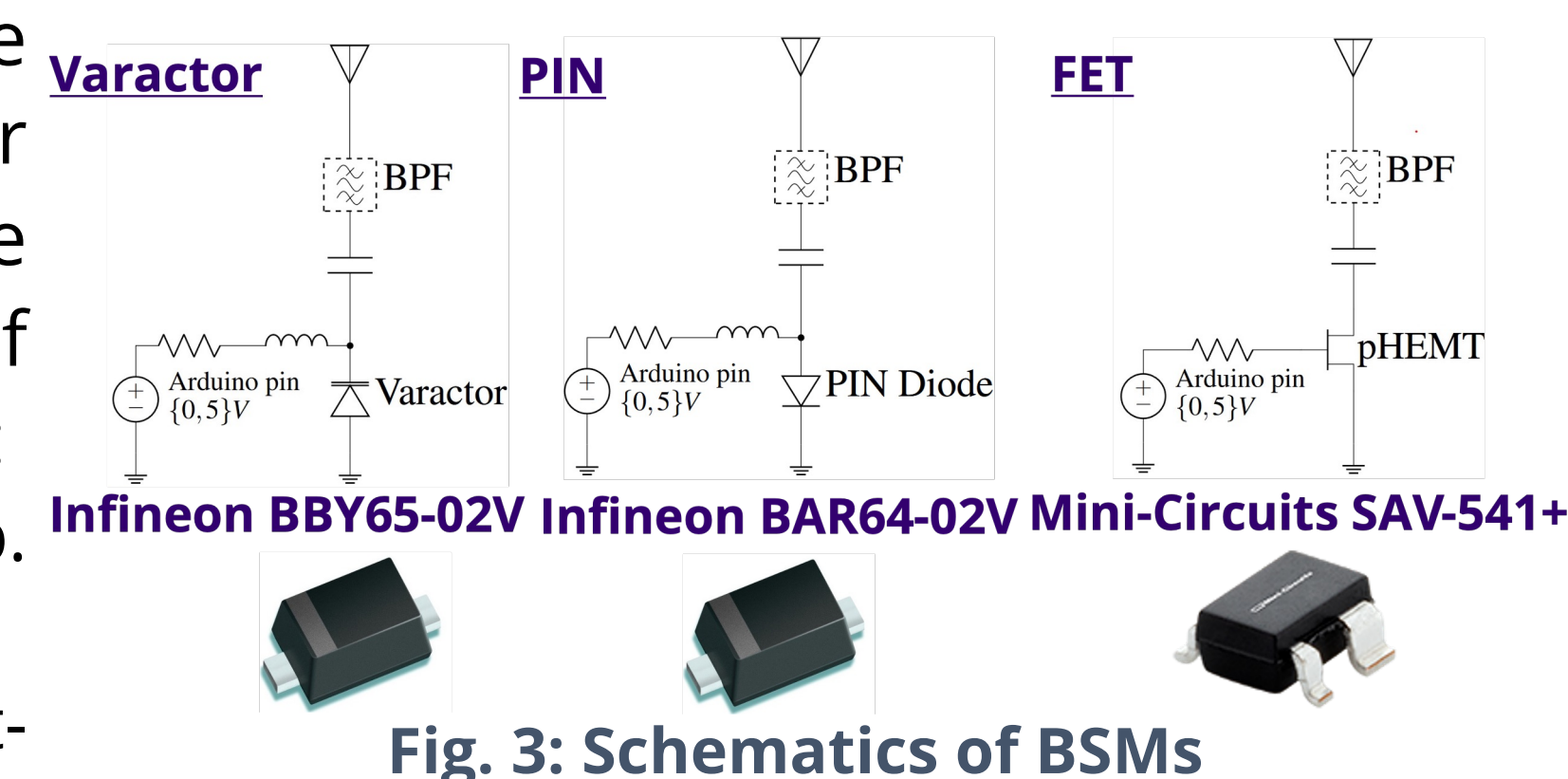


Fig. 3: Schematics of BSMs

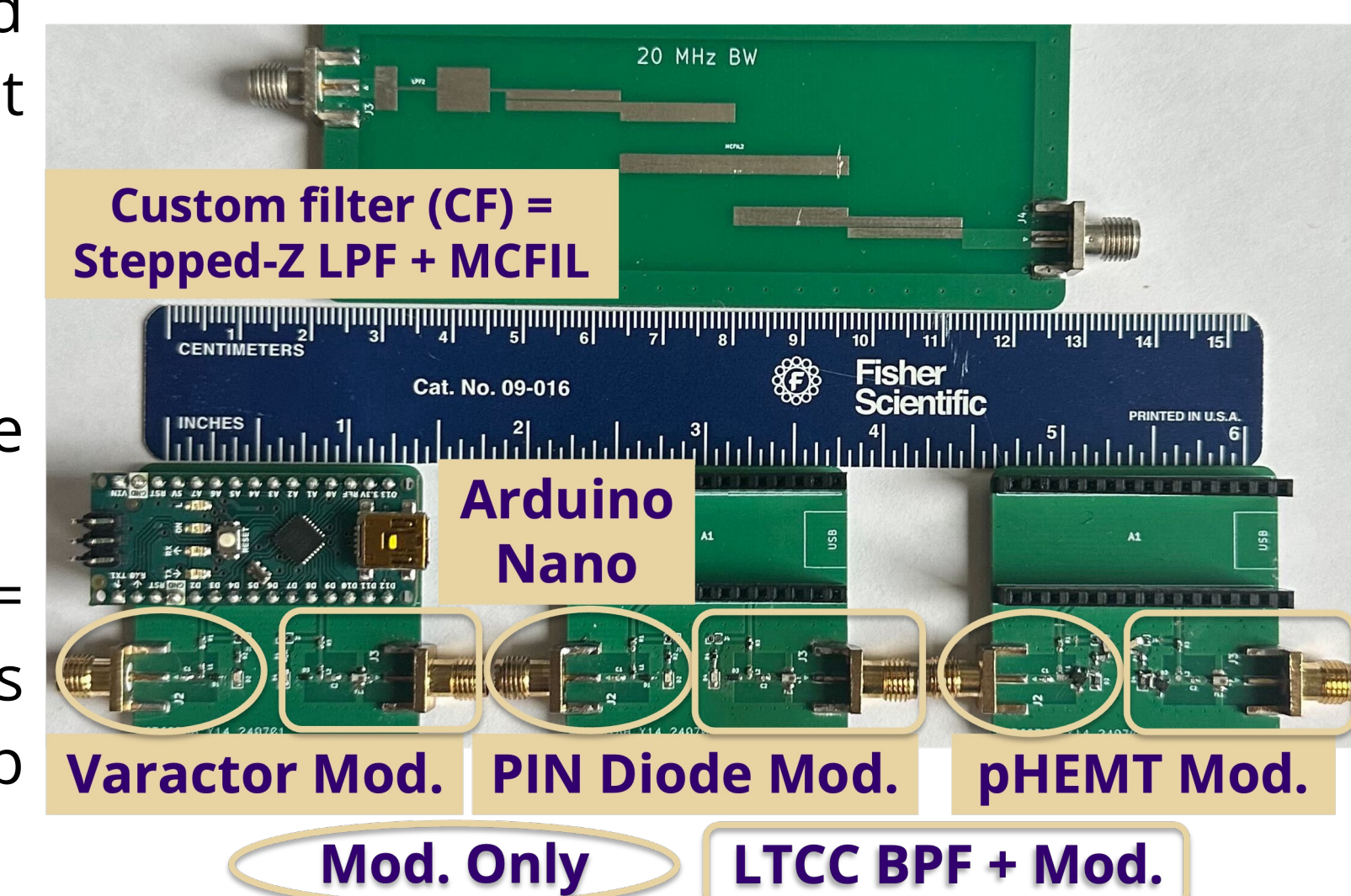


Fig. 4: Photo of PCBs

Table I: Meas. Mod. Power Consumption at 1 Mbps

Modulator Device	Avg. Power Consumption	Energy Efficiency
pHEMT	1.90 $\mu$ W	1.90 pJ/bit
Varactor	46.25 $\mu$ W	46.25 pJ/bit
PIN Diode	22.30 mW	22.30 nJ/bit

## Measured vs Simulated Results

- A calibrated vector network analyzer was used to measure the two reflection coefficients of each modulator from 0.5–8.5 GHz →  $|\Delta\Gamma_{50\Omega}|$  and  $|\Delta\Gamma_A|$  determined from measurements as discussed previously
- Simulations were conducted in AWR Microwave Office
- Good qualitative agreement between meas. and sim., especially at lower frequencies. At higher frequencies, FR-4 substrate loss becomes a limiting factor

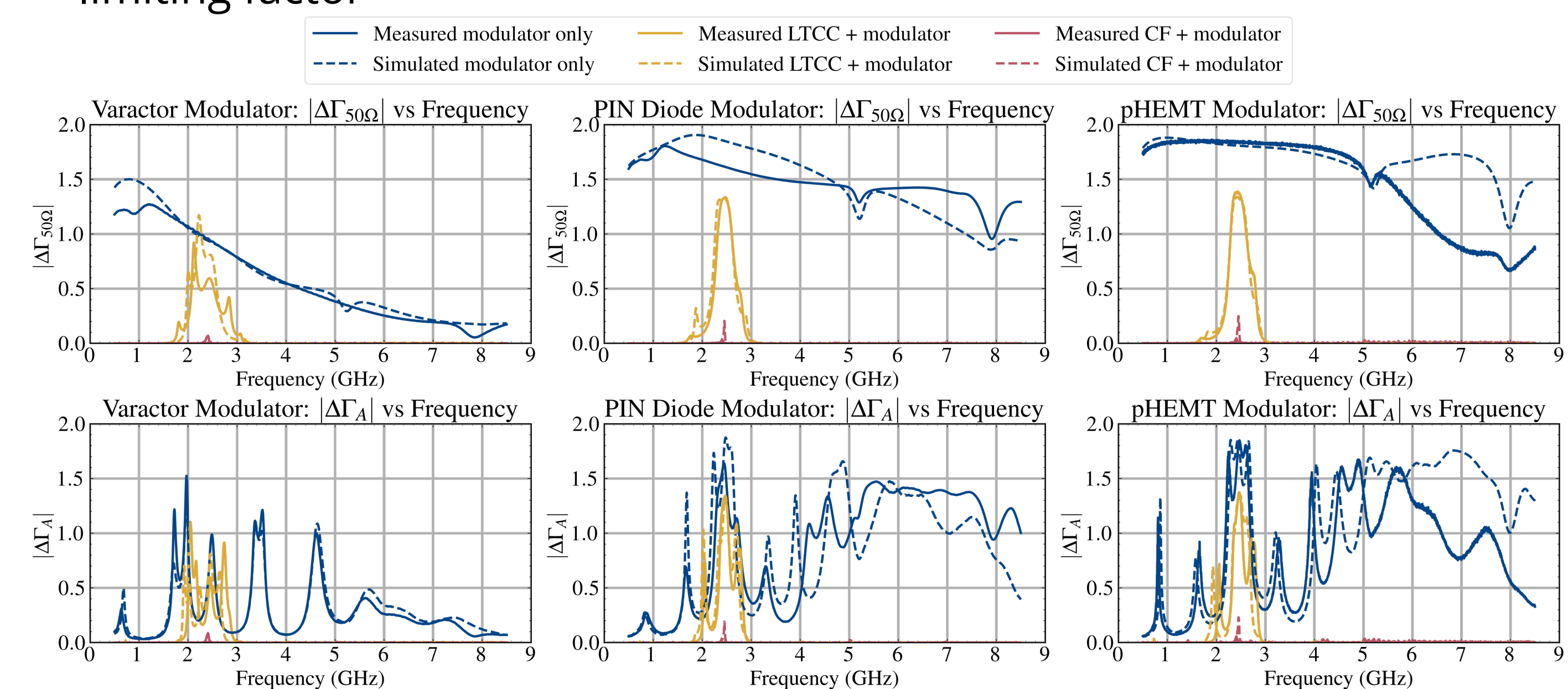


Fig. 5: Measured vs simulated  $|\Delta\Gamma_{50\Omega}|$  and  $|\Delta\Gamma_A|$  for modulator variants

Table II: Summary of Measured Key Metrics

Metric	Modulator Only			LTCC BPF + Modulator			CF + Modulator		
	Var.	PIN	pHEMT	Var.	PIN	pHEMT	Var.	PIN	pHEMT
Peak $ \Delta\Gamma_{50\Omega} $ , 2400-2483 MHz	0.960	1.622	1.849	0.596	1.328	1.385	0.069	0.036	0.047
$ \Delta\Gamma_{50\Omega} $ 3dB mod. BW (MHz)	3416	7730	5856	510	308	328	50	30	28
Peak $ \Delta\Gamma_{50\Omega} $ , 4900-7200 MHz	0.396	1.437	1.655	0.004	0.003	0.004	0.003	0.007	0.025
Peak $ \Delta\Gamma_A $ , 2400-2483 MHz	0.986	1.638	1.849	0.594	1.328	1.373	0.086	0.036	0.057
$ \Delta\Gamma_A $ 3dB mod. BW (MHz)	110	269	322	87	176	183	36	27	27
Peak $ \Delta\Gamma_A $ , 4900-7200 MHz	0.407	1.471	1.672	0.005	0.004	0.006	0.004	0.007	0.033

- Modulator only:** high  $|\Delta\Gamma|$  within 2.4 GHz ISM band, but also within antenna's higher passbands from 4900-7200 MHz
  - LTCC BPF + Modulator:** added filter eliminates  $|\Delta\Gamma|$  in antenna's higher passbands, and reduces the 3dB modulation BW ( $\Delta\Gamma_{3dB}$ )
  - CF + Modulator:** narrower  $\Delta\Gamma_{3dB}$ , but severely reduced in-band  $|\Delta\Gamma|$
- Overall,** varactor has lowest  $|\Delta\Gamma|$ ; PIN and pHEMT exhibit similar  $|\Delta\Gamma|$  levels, with drawback of higher power consumption or cost, respectively.

## Next Steps

- Narrow modulation bandwidth further using reduced-size purpose-built filters, e.g. surface acoustic wave (SAW) or bulk acoustic wave (BAW) filters
- Validate approach using higher order modulation schemes and/or in other communications bands

## Acknowledgments and References

<sup>1</sup>Unhelkar et al., *IJIM Data Insights*, 2022. <sup>2</sup>Toro et al., *IEEE Trans. Green Commun. Netw.*, 2022. <sup>3</sup>Rosenthal et al., *IEEE Trans. Microw. Theory Techn.*, 2019. <sup>4</sup>Thomas et al., *ACM SIGCOMM*, 2012. <sup>5</sup>Alhassoun, *IEEE Access*, 2023.